

# Probabilistic Nonlinear Finite Element Analysis of Reinforced Concrete Beams without Shear Reinforcement

MSc graduation Thesis  
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Civil Engineering  
Geotechnical Engineering  
Petroleum Engineering



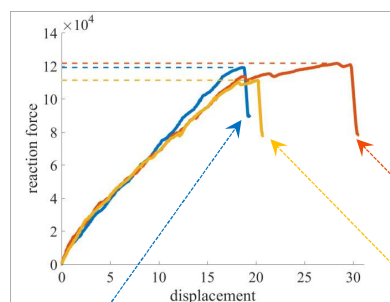
2016, November 24

## Problem definition

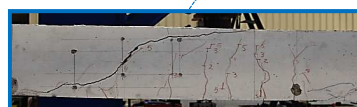
### Experimental results

- similar experiments
- different failure mode

⇒ material uncertainty



beam A – flexural failure



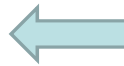
beam B – shear failure



beam C – shear failure

## Research objectives

- Tackle the effect of material uncertainty
- Explain the bi-modal experimental behavior.
- Estimate reliability measures.

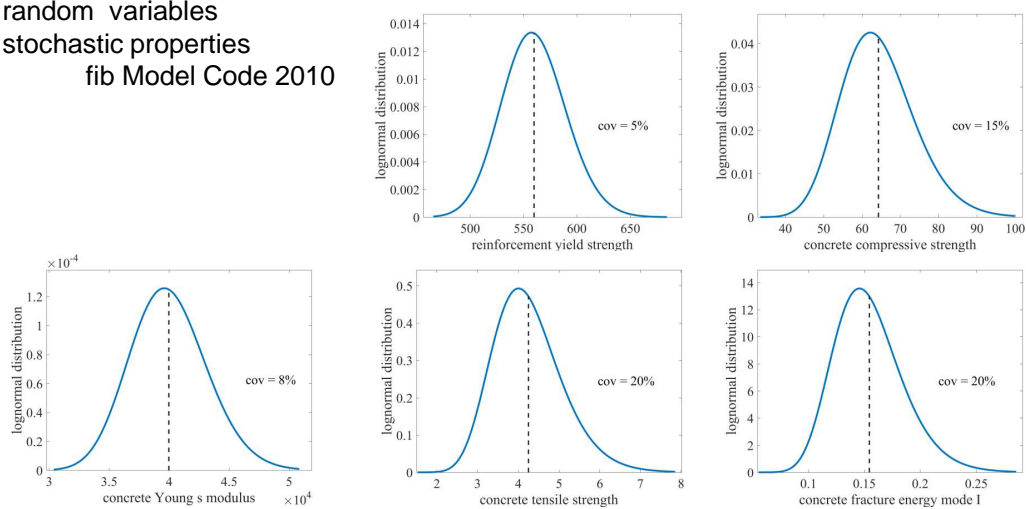


### Solution strategy

- stochastic approach
- structural analysis
- quantify material uncertainty

## Quantifying the material uncertainty

- random variables
- stochastic properties  
fib Model Code 2010

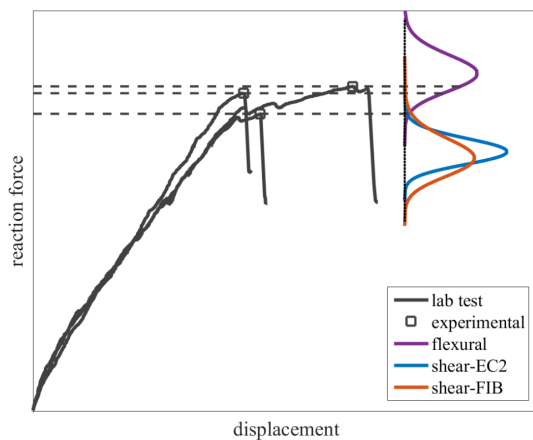


## Solution strategy

- structural analysis
  - analytical models EC2  
Model Code
  - finite element modeling
- stochastic approach

## Analytical models

Analytical models vs Experimental data



- Monte Carlo Simulation

- analytical models
  - shear capacity
  - flexural capacity

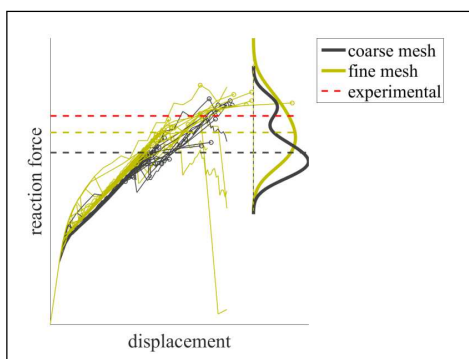


- higher prob. of occurrence:  
shear failure
- failure mode transition

## Solution strategy

- structural analysis
  - analytical models ~~EC2~~  
~~Model Code~~
  - finite element modeling      calibration
- stochastic approach

## Calibrating the FE model – numerical scheme



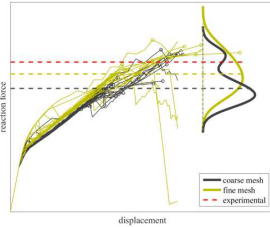
- mean material properties
- convergence
- stability
- vs experimental results
  - failure mode
  - accuracy

Numerical scheme	Mesh		Load		Convergence		Iterative scheme		
	aspect ratio	element size	type	step size	norm	tol.	iterations	stiffness	conver. scheme
final scheme	1	25	displa.	2.5%	energy	$1e-03$	400	secant	line-search

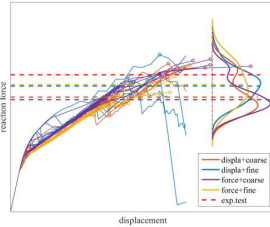
Scheme	Mesh		Load		Convergence		Iterative scheme		
	aspect ratio	element size	type	step size	norm	tol.	iterations	stiffness	conver. scheme
scheme0	1	25	displa.	5%	displa	$1e-02$	400	secant	line-search
		50	force	1%	energy	$1e-03$			
					force	$1e-02$			
					force & displa.	$1e-03$			

## Calibrating the FE model – numerical scheme

mesh

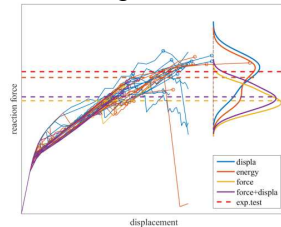


control

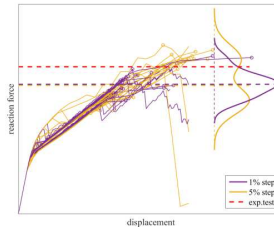


Scheme	Mesh		Load		Convergence		Iterative scheme		
	aspect ratio	element size	type	step size	norm	tol.	iterations	stiffness	conver. scheme
scheme0	1	25	displa.	5%	displa	$1e-02$	400	secant	line-search
						$1e-03$			
		50	force	1%	energy	$1e-04$		Newton-Raphson	arc-length
					force	$1e-03$			
					force & displa.	$1e-02$			
						$1e-03$			

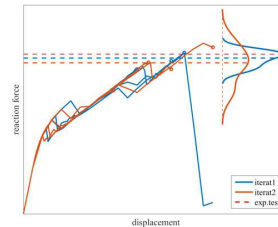
convergence norm



load increments size



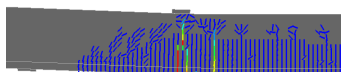
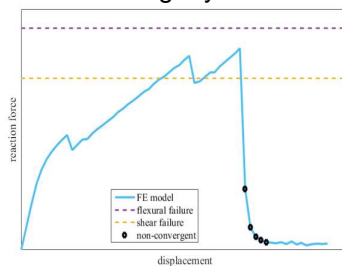
iterative method



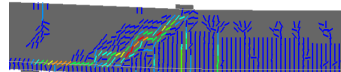
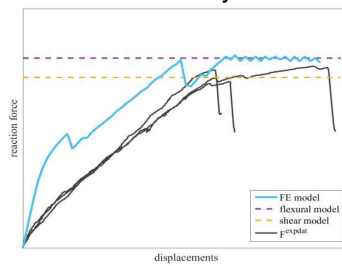
## Calibrating the FE model – constitutive scheme

Constitutive behavior	Concrete							Steel			
	tension soften.	compress. soften.	total crack strain	shear retention	reduction Poisson	lateral confine.	lateral cracking.	$\sigma - \epsilon$	concrete - reinforcement	concrete-steel	$\sigma - \epsilon$
FE model	hordijk	parabolic	fixed	damage based	damage based	Selby & Vecchio	Vecchio & Collins	von Mises	embedded	interface	linear

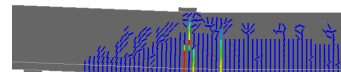
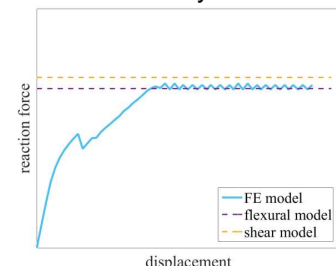
high fy



mean fy



low fy



## Solution strategy

- structural analysis

- analytical models ~~EC2~~  
~~Model Code~~

- finite element modeling calibration

- stochastic approach

- semi-probabilistic: ~~partial safety factor~~  
~~global safety factor~~

- full probabilistic ~~Monte Carlo~~  
Response Surface Method

PNLFEA

DIANA 10.0 – PROBAB

Directional Adaptive  
Response Surface method  
(DARS)

## Input for PNLFEA

- random variables, (**X**)

- concrete:  $p=1.00$

- finite element model

(calibrated)

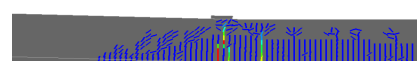
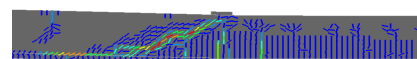
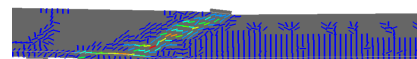
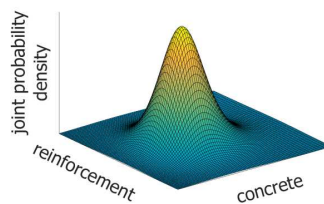
- method

- Directional Adaptive  
Response Surface (**DARS**)

- analysis parameters

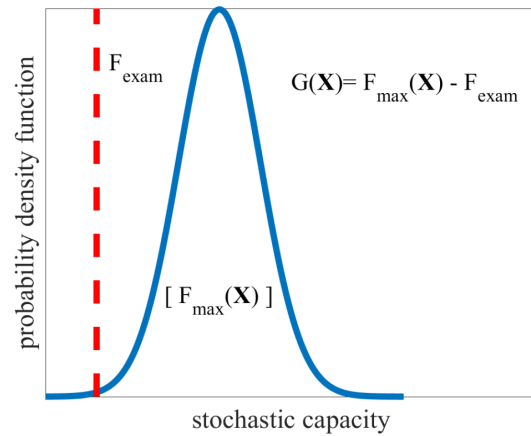
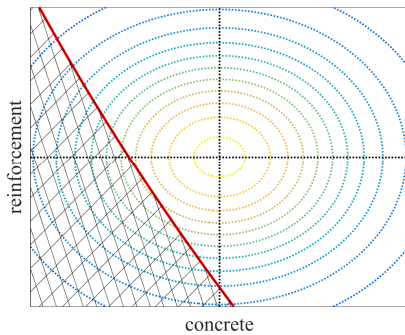
- number of samples, tolerances, etc

- limit state function



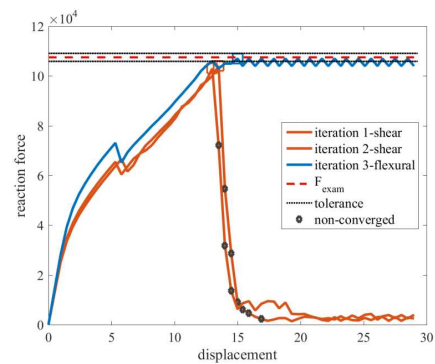
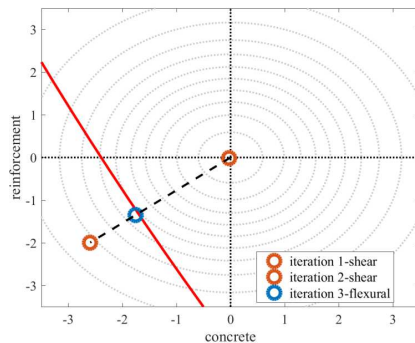
## Limit state function

- reaction force capacity  $G(\mathbf{X}) = F_{\max}(\mathbf{X}) - F_{\text{exam}}$
- limit state function,  $G(\mathbf{X})$ 
  - $G(\mathbf{X}) > 0$ , safe
  - $G(\mathbf{X}) \leq 0$ , failure



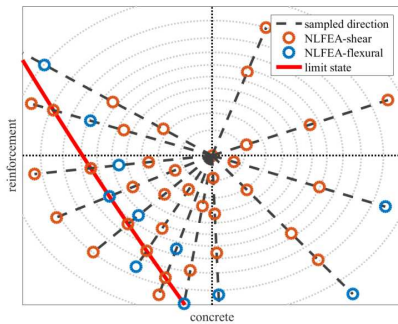
## PNLFEA - DARS

- directional sampling & line search
- NLFEA

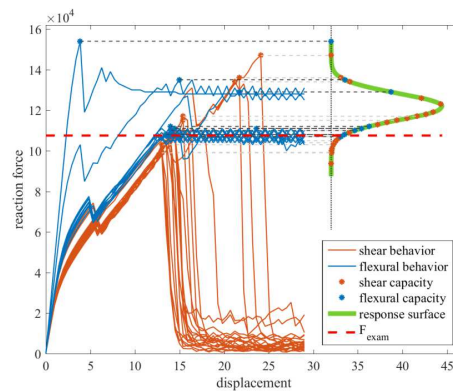


## PNLFEA - DARS

- directional sampling & line search



- NLFEA



- fitting the response surface function

$$G^*(U) = a + \sum_{i=1}^n b_i U_i + \sum_{i=1}^n c_i U_i^2 = a + b_1 U_c + b_2 U_y + c_1 U_c^2 + c_2 U_y^2$$

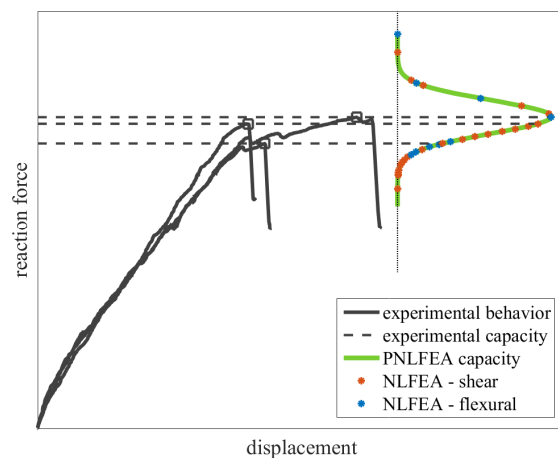
## PNLFEA vs Experimental results

- PNLFEA (RS)

⇒ full structural behavior

- PNLFEA vs Experimental results
  - capacity
  - failure mode

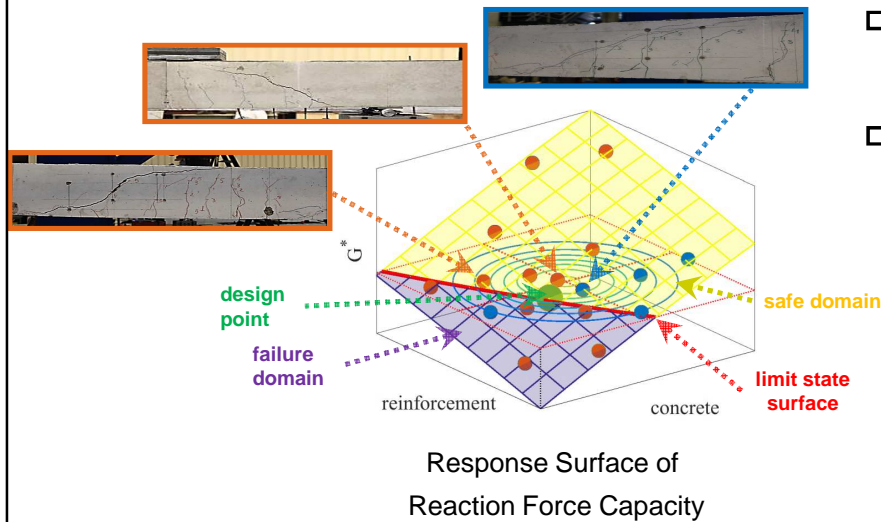
⇒ bi-modal experimental behavior





## Response surface & Reliability

- Monte Carlo on Response Surface Function



$$\beta = 2.22$$

$$P_f = 0.0131$$

$$P_{oc.shear} = 76.34\%$$

$$P_{oc.flexural} = 23.66\%$$

⇒ actual material properties

⇒ design point

## Sensitivity measures

- correlation between concrete properties: ( $\rho=0.85$ )
- constructed response surface function:

$$G^*(U) = 0.135 - 0.838 \cdot 10^{-5} \cdot U_{f_c} + 0.562 \cdot 10^{-2} \cdot U_{f_{ct}} - 0.329 \cdot 10^{-4} \cdot U_{G_f^l}$$

$$- 0.586 \cdot 10^{-5} \cdot U_{E_c} - 0.386 \cdot 10^{-2} \cdot U_{f_y}$$

$$- 0.134 \cdot 10^{-4} \cdot U_{f_c}^2 - 0.692 \cdot 10^{-4} \cdot U_{f_{ct}}^2 - 0.133 \cdot 10^{-4} \cdot U_{G_f^l}^2$$

$$- 0.132 \cdot 10^{-4} \cdot U_{E_c}^2 + 0.257 \cdot 10^{-4} \cdot U_{f_y}^2$$

- largest influence
  - concrete tensile strength
  - reinforcement yield strength

## Conclusions

- Explain the experimentally observed behavior of reinforced concrete beams without shear reinforcement
  - actual material properties of experimental members
- Tackle the effect of material uncertainty
  - structural behavior for all realizations of material properties
  - sensitivity measures
- Estimate reliability measures
  - structural reliability
  - probability of occurrence of each failure mode
  - design point

## Current improvements

- Response surface function
  - cross-terms
  - multiple limit states
  - multiple design-points
  - higher efficiency/robustness

$$G = a + \sum_{i=1}^n b_i u_i + \sum_{i=1}^n c_i u_i^2 + \sum_{i=1}^n \sum_{j=1, j \neq i}^n d_{ij} u_i u_j$$

- Model uncertainty factor
  - $\theta$
  - FEM uncertainty
  - higher robustness

$$G(\mathbf{X}, \boldsymbol{\theta}) = \boldsymbol{\theta} F_{\max}(\mathbf{X}) - F_{\text{exam}}$$

## Application

- Wide range of application
  - all FEM applications
  - random variables: material, geometrical, loading
  - multiple limit states: reaction force, stress, strain, displacement, etc
  - examination + design purposes
- Reinforced concrete bridges designed with old structural codes
- Advantages
  - full probabilistic: all scenarios considered
  - finite element analysis: advanced analysis, system effects

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