

Probabilistic Nonlinear Finite Element Analysis of Reinforced Concrete Beams without Shear Reinforcement

MSc graduation Thesis
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Civil Engineering
Geotechnical Engineering
Petroleum Engineering



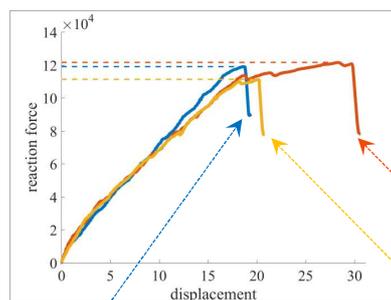
2016, November 24

Problem definition

Experimental results

- similar experiments
- different failure mode

⇒ material uncertainty



beam A – flexural failure



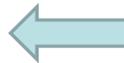
beam B – shear failure



beam C – shear failure

Research objectives

- Tackle the effect of material uncertainty
- Explain the bi-modal experimental behavior.
- Estimate reliability measures.

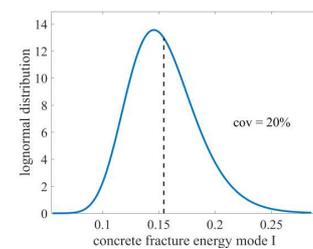
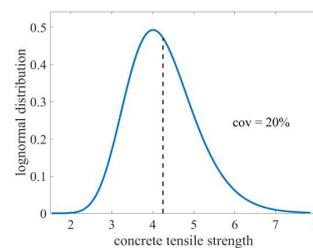
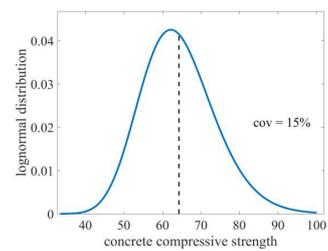
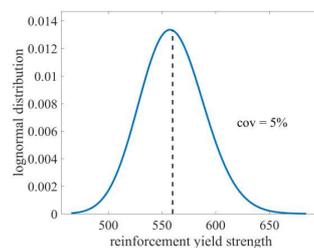
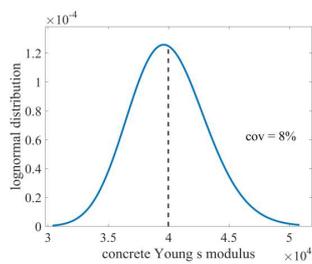


Solution strategy

- stochastic approach
- structural analysis
- quantify material uncertainty

Quantifying the material uncertainty

- random variables
- stochastic properties
fib Model Code 2010

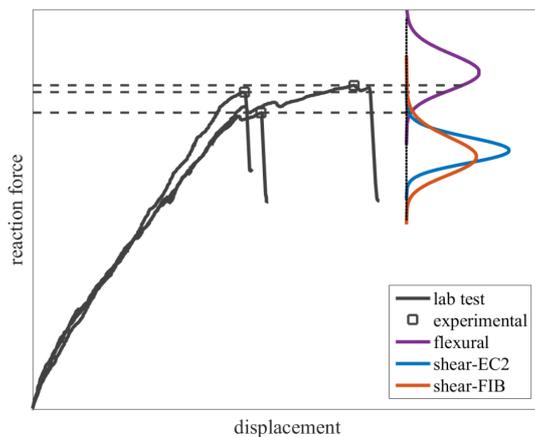


Solution strategy

- structural analysis
 - analytical models EC2 Model Code
 - finite element modeling
- stochastic approach

Analytical models

Analytical models vs Experimental data



- Monte Carlo Simulation
- analytical models
 - shear capacity
 - flexural capacity

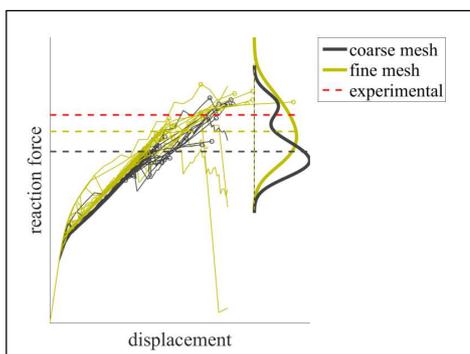


- higher prob. of occurrence: shear failure
- failure mode transition

Solution strategy

- structural analysis
 - analytical models ~~EC2~~
~~Model Code~~
 - finite element modeling calibration
- stochastic approach

Calibrating the FE model – numerical scheme



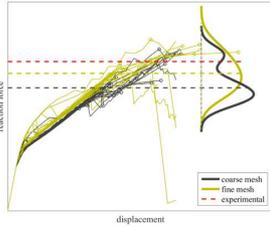
- mean material properties
- convergence
- stability
- vs experimental results
 - failure mode
 - accuracy

Numerical scheme	Mesh		Load		Convergence		Iterative scheme		
	aspect ratio	element size	type	step size	norm	tol.	iterations	stiffness	conver. scheme
final scheme	1	25	displa.	2.5%	energy	1e-03	400	secant	line-search
		50	force	1%	energy	1e-03	400	Newton-Raphson	arc-length

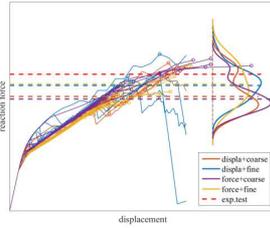
Scheme	Mesh		Load		Convergence		Iterative scheme		
	aspect ratio	element size	type	step size	norm	tol.	iterations	stiffness	conver. scheme
scheme0	1	25	displa.	5%	displa	1e-02	400	secant	line-search
		50	force	1%	energy	1e-03	400	Newton-Raphson	arc-length
final scheme	1	25	displa.	2.5%	energy	1e-03	400	secant	line-search

Calibrating the FE model – numerical scheme

mesh

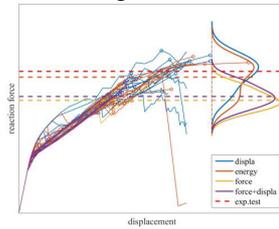


control

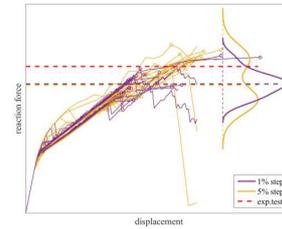


Scheme	Mesh		Load			Convergence		Iterative scheme		
	aspect ratio	element size	type	step size	norm	tol.	iterations	stiffness	conver. scheme	
scheme0	1	25	displa.	5%	displa	1e-02	400	secant	line-search	
		50	force	1%	energy	1e-04		Newton-Raphson	arc-length	
					force	1e-02				
					force & displa.	1e-03				

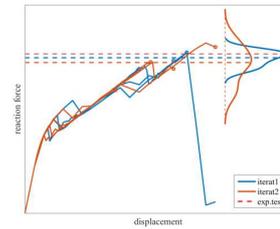
convergence norm



load increments size



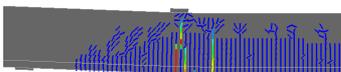
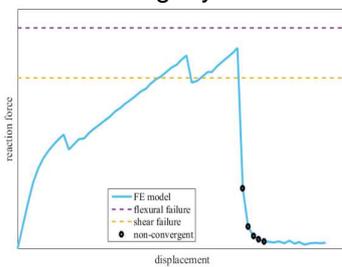
iterative method



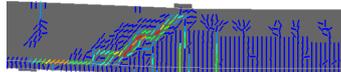
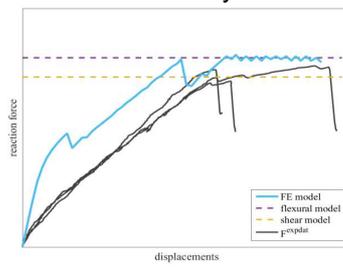
Calibrating the FE model – constitutive scheme

Constitutive behavior	Concrete							Steel			
	tension soften.	compress. soften.	total crack strain	shear retention	reduction Poisson	lateral confine.	lateral cracking.	$\sigma - \epsilon$	concrete - reinforcement	concrete-steel	$\sigma - \epsilon$
FE model	hordijk	parabolic	fixed	damage based	damage based	Selby & Vecchio	Vecchio & Collins	von Mises	embedded	interface	linear

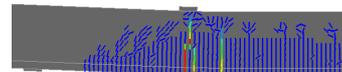
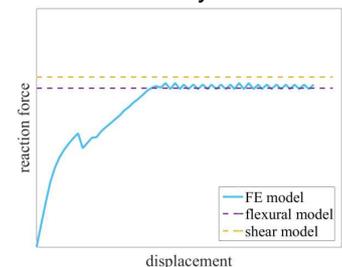
high fy



mean fy



low fy



Solution strategy

- structural analysis

- analytical models ~~EC2~~
~~Model Code~~

- finite element modeling calibration

- stochastic approach

- semi-probabilistic: ~~partial safety factor~~
~~global safety factor~~

- full probabilistic ~~Monte Carlo~~
Response Surface Method

PNLFEA

DIANA 10.0 – PROBAB

Directional Adaptive
Response Surface method
(DARS)

Input for PNLFEA

- random variables, (**X**)

- concrete: $\rho=1.00$

- finite element model

(calibrated)

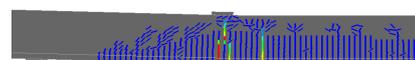
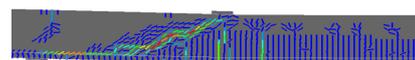
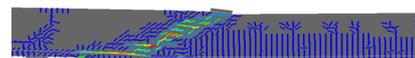
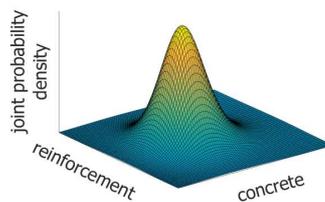
- method

- Directional Adaptive
Response Surface (**DARS**)

- analysis parameters

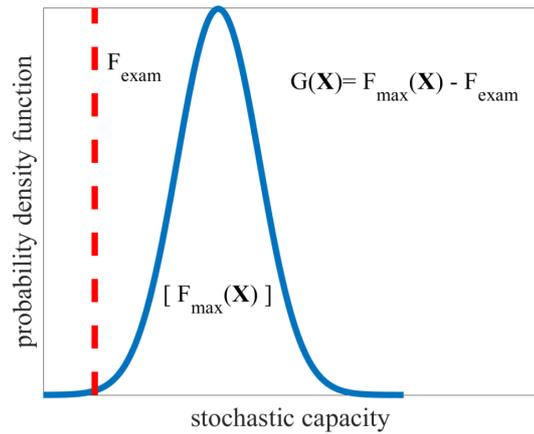
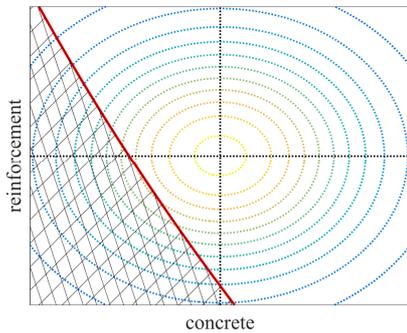
- number of samples, tolerances, etc

- limit state function



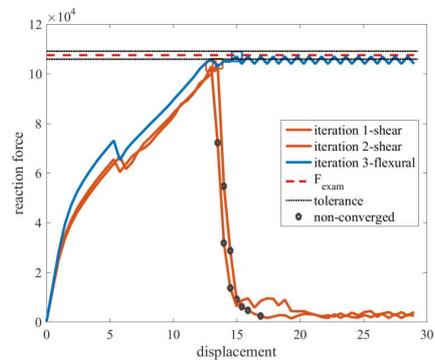
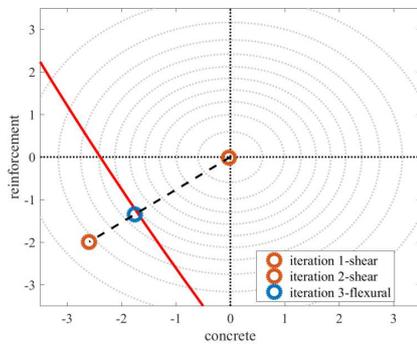
Limit state function

- reaction force capacity $G(\mathbf{X}) = F_{\max}(\mathbf{X}) - F_{\text{exam}}$
- limit state function, $G(\mathbf{X})$
 - $G(\mathbf{X}) > 0$, safe
 - $G(\mathbf{X}) \leq 0$, failure



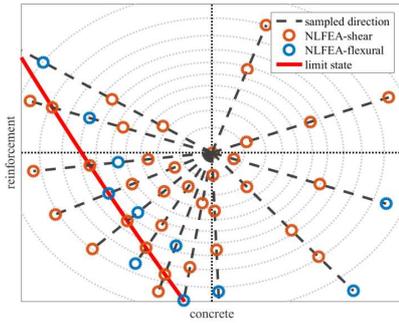
PNLFEA - DARS

- directional sampling & line search
- NLFEA

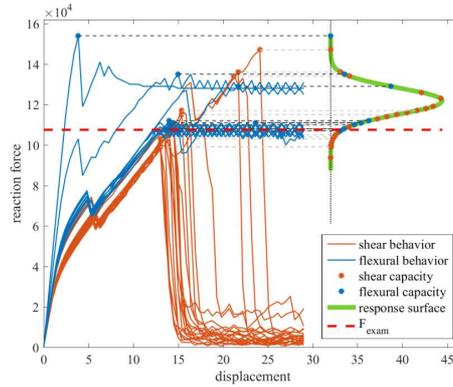


PNLFEA - DARS

- directional sampling & line search



- NLFEA



- fitting the response surface function

$$G^*(U) = a + \sum_{i=1}^n b_i U_i + \sum_{i=1}^n c_i U_i^2 = a + b_1 U_c + b_2 U_y + c_1 U_c^2 + c_2 U_y^2$$

PNLFEA vs Experimental results

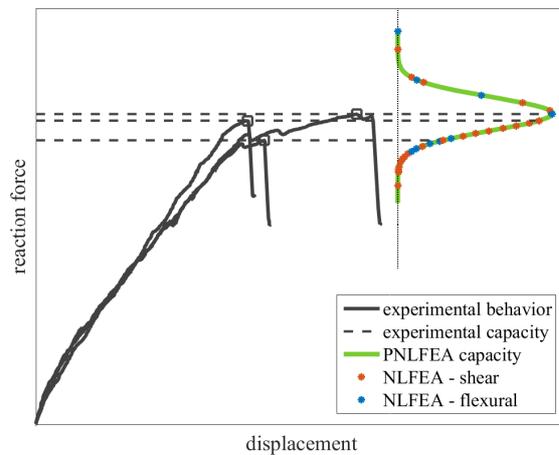
- PNLFEA (RS)

⇒ full structural behavior

- PNLFEA vs Experimental results

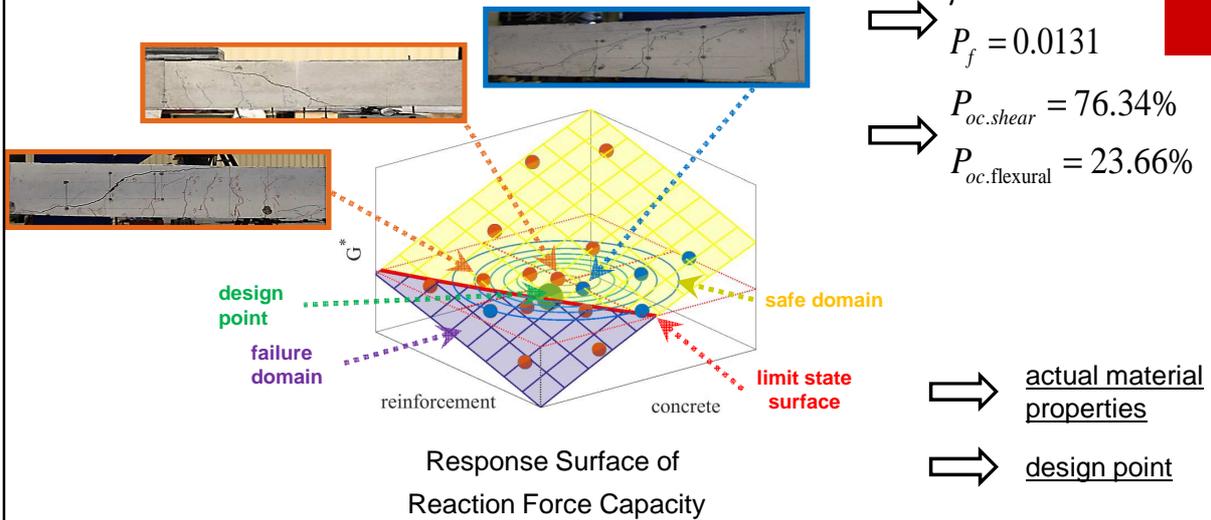
- capacity
- failure mode

⇒ bi-modal experimental behavior



Response surface & Reliability

- Monte Carlo on Response Surface Function



Sensitivity measures

- correlation between concrete properties: ($\rho=0.85$)
- constructed response surface function:

$$\begin{aligned}
 G^*(\mathbf{U}) = & 0.135 - 0.838 \cdot 10^{-5} \cdot U_{f_c} + 0.562 \cdot 10^{-2} \cdot U_{f_{ct}} - 0.329 \cdot 10^{-4} \cdot U_{G_f^l} \\
 & - 0.586 \cdot 10^{-5} \cdot U_{E_c} - 0.386 \cdot 10^{-2} \cdot U_{f_y} \\
 & - 0.134 \cdot 10^{-4} \cdot U_{f_c}^2 - 0.692 \cdot 10^{-4} \cdot U_{f_{ct}}^2 - 0.133 \cdot 10^{-4} \cdot U_{G_f^l}^2 \\
 & - 0.132 \cdot 10^{-4} \cdot U_{E_c}^2 + 0.257 \cdot 10^{-4} \cdot U_{f_y}^2
 \end{aligned}$$

- largest influence
 concrete tensile strength
 reinforcement yield strength

Conclusions

- Explain the experimentally observed behavior of reinforced concrete beams without shear reinforcement
 - actual material properties of experimental members
- Tackle the effect of material uncertainty
 - structural behavior for all realizations of material properties
 - sensitivity measures
- Estimate reliability measures
 - structural reliability
 - probability of occurrence of each failure mode
 - design point

Current improvements

- Response surface function
 - cross-terms
 - multiple limit states
 - multiple design-points
 - higher efficiency/robustness

$$G = a + \sum_{i=1}^n b_i u_i + \sum_{i=1}^n c_i u_i^2 + \sum_{i=1}^n \sum_{j=1, j \neq i}^n d_{ij} u_i u_j$$

- Model uncertainty factor
 - θ
 - FEM uncertainty
 - higher robustness

$$G(\mathbf{X}, \theta) = \theta F_{\max}(\mathbf{X}) - F_{exam}$$

Application

- Wide range of application
 - all FEM applications
 - random variables: material, geometrical, loading
 - multiple limit states: reaction force, stress, strain, displacement, etc
 - examination + design purposes
- Reinforced concrete bridges designed with old structural codes
- Advantages
 - full probabilistic: all scenarios considered
 - finite element analysis: advanced analysis, system effects

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